# Precision Air-Core Tach/Speedo Driver with Short Circuit Protection 

The CS8191 is specifically designed for use with 4 quadrant air-core meter movements. The IC includes an input comparator for sensing input frequency such as vehicle speed or engine RPM, a charge pump for frequency to voltage conversion, a bandgap reference for stable operation and a function generator with sine and cosine
amplifiers that differentially drive the motor coils.
The CS8191 has a higher torque output and better output signal symmetry than other competitive parts (CS289, and LM1819). It is protected against short circuit and overvoltage ( 60 V ) fault conditions. Enhanced circuitry permits functional operation down to 8 V .

| Absolute Maximum Ratings |  |
| :---: | :---: |
| Supply Voltage | $\begin{aligned} & \left(\leq 100 \mathrm{~ms} \text { pulse transient) ........................................................................................... } \mathrm{V}_{\mathrm{CC}}=24 \mathrm{~V}\right. \end{aligned}$ |
| Operating Temperature Range ............................................. - $^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ |  |
| Junction Temperature Range ........................................... $-40^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |  |
| Storage Temperature Range................................................- $55^{\circ} \mathrm{C}$ to $+165^{\circ} \mathrm{C}$ |  |
| Electrostatic Discharge (Human Body Model).......................................... 4 kVLead Temperature Soldering |  |
|  |  |
| Wave Solder (through hole styles only) $\qquad$ .10 sec. max, $260^{\circ} \mathrm{C}$ peak Reflow (SMD styles only) $\qquad$ .60 sec. max above $183^{\circ} \mathrm{C}, 230^{\circ} \mathrm{C}$ peak |  |
|  |  |

Block Diagram


## Features

Direct Sensor Input

- High Output Torque

Wide Output Voltage Range

- High Impedance Inputs
- Accurate down to $10 \mathrm{~V} \mathrm{~V}_{\mathrm{CC}}$

Fault Protection
Overvoltage
Short Circuit
Low Voltage Operation
Package Options
16 Lead PDIP (internally fused leads)


## ■ Supply Voltage Section

| $\mathrm{I}_{\mathrm{CC}}$ Supply Current | $\mathrm{V}_{\mathrm{CC}}=16 \mathrm{~V},-40^{\circ} \mathrm{C}$, No Load |  | 70 | 125 | mA |
| :--- | :--- | :---: | :---: | :---: | :---: |
| $\mathrm{~V}_{\mathrm{CC}}$ Normal Operation Range |  | 8.0 | 13.1 | 16.0 | V |

## Input Comparator Section

| Positive Input Threshold |  |  | 2.4 | 2.7 | 3.0 | V |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Negative Input Threshold |  | 2.0 | 2.3 |  | V |  |
| Input Hysteresis |  | 200 | 400 | 1000 | mV |  |
| Input Bias Current $*$ | $0 \mathrm{~V} \leq \mathrm{V}_{\mathrm{IN}} \leq 8 \mathrm{~V}$ |  | -2 | $\pm 10$ | $\mu \mathrm{~A}$ |  |
| Input Frequency Range |  | 0 |  | 20 | kHz |  |
| Input Voltage Range | in series with $1 \mathrm{k} \Omega$ | -1 |  | $\mathrm{~V}_{\mathrm{CC}}$ | V |  |
| Output $\mathrm{V}_{\mathrm{SAT}}$ | $\mathrm{I}_{\mathrm{CC}}=10 \mathrm{~mA}$ |  | 0.15 | 0.40 | V |  |
| Output Leakage | $\mathrm{V}_{\mathrm{CC}}=7 \mathrm{~V}$ |  |  |  | 10 | $\mu \mathrm{~A}$ |
| Logic 0 Input Voltage |  |  |  |  | V |  |

*Note: Input is clamped by an internal 12 V Zener.

## ■ Voltage Regulator Section

| Output Voltage |  | 6.50 | 7.00 | 7.50 | V |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Output Load Current |  |  |  | 10 | mA |
| Output Load Regulation | 0 to 10 mA |  | 10 | 50 | mV |
| Output Line Regulation | $8.0 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 16 \mathrm{~V}$ |  | 20 | 150 | mV |
| Power Supply Rejection | $\mathrm{V}_{\mathrm{CC}}=13.1 \mathrm{~V}, 1 \mathrm{~V}_{\mathrm{P}} / \mathrm{P} 1 \mathrm{kHz}$ | 34 | 46 |  | dB |
| ■ Charge Pump Section |  |  |  |  |  |
| Inverting Input Voltage |  | 1.5 | 2.0 | 2.5 | V |
| Input Bias Current |  |  | 40 | 150 | nA |
| $\mathrm{V}_{\text {BIAS }}$ Input Voltage |  | 1.5 | 2.0 | 2.5 | V |
| Non Invert. Input Voltage | $\mathrm{I}_{\mathrm{IN}}=1 \mathrm{~mA}$ |  | 0.7 | 1.1 | V |
| Linearity* | @ 0, 87.5, 175, 262.5, + 350Hz | -0.10 | 0.28 | +0.70 | \% |
| F/V $\mathrm{V}_{\text {OUT }}$ Gain | @ $350 \mathrm{~Hz}, \mathrm{C}_{\mathrm{T}}=0.0033 \mu \mathrm{~F}, \mathrm{R}_{\mathrm{T}}=243 \mathrm{k} \Omega$ | 7 | 10 | 13 | $\mathrm{mV} / \mathrm{Hz}$ |
| Norton Gain, Positive | $\mathrm{I}_{\text {IN }}=15 \mu \mathrm{~A}$ | 0.9 | 1.0 | 1.1 | I/I |
| Norton Gain, Negative | $\mathrm{I}_{\mathrm{IN}}=-15 \mu \mathrm{~A}$ | 0.9 | 1.0 | 1.1 | I/I |

*Note: Applies to \% of full scale ( $270^{\circ}$ ).

## $\square$ Function Generator Section: $-40^{\circ} \leq \mathrm{T}_{\mathrm{A}} \leq 85^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}}=13.1 \mathrm{~V}$ unless otherwise noted.

| Differential Drive Voltage $\left(\mathrm{V}_{\mathrm{COS}^{+}}-\mathrm{V}_{\mathrm{COS}^{-}}\right)$ | $\begin{aligned} & 10 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 16 \mathrm{~V} \\ & \Theta=0^{\circ} \end{aligned}$ | 7.5 | 8.0 | 8.5 | V |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Differential Drive Voltage $\left(\mathrm{V}_{\mathrm{SIN}^{+}}-\mathrm{V}_{\mathrm{SIN}^{-}}\right)$ | $\begin{aligned} & 10 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 16 \mathrm{~V} \\ & \Theta=90^{\circ} \end{aligned}$ | 7.5 | 8.0 | 8.5 | V |
| Differential Drive Voltage $\left(\mathrm{V}_{\mathrm{COS}^{+}}-\mathrm{V}_{\mathrm{COS}^{-}}\right)$ | $\begin{aligned} & 10 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 16 \mathrm{~V} \\ & \Theta=180^{\circ} \end{aligned}$ | -8.5 | -8.0 | -7.5 | V |
| Differential Drive Voltage $\left(\mathrm{V}_{\mathrm{SIN}^{+}}-\mathrm{V}_{\mathrm{SIN}^{-}}\right)$ | $\begin{aligned} & 10 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 16 \mathrm{~V} \\ & \Theta=270^{\circ} \end{aligned}$ | -8.5 | -8.0 | -7.5 | V |
| Differential Drive Load | $10 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 16 \mathrm{~V},-40^{\circ} \mathrm{C}$ | 178 |  |  | $\Omega$ |
|  | $25^{\circ} \mathrm{C}$ | 239 |  |  | $\Omega$ |
|  | $105^{\circ} \mathrm{C}$ | 314 |  |  | $\Omega$ |
| Zero Hertz Output Voltage |  | -0.08 | 0.0 | +0.08 | V |


| Electrical Characteristics: continued |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| - Function Generator Section: continued |  |  |  |  |  |
| Function Generator Error * | $\Theta=0^{\circ}$ to $225^{\circ}$ | -2 | 0 | +2 | deg |
| Reference Figures 1-4 | $\Theta=226^{\circ}$ to $305^{\circ}$ | -3 | 0 | +3 | deg |
| Function Generator Error | $13.1 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 16 \mathrm{~V}$ | -1 | 0 | +1 | deg |
| Function Generator Error | $13.1 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 10 \mathrm{~V}$ | -1 | 0 | +1 | deg |
| Function Generator Error | $13.1 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 8.0 \mathrm{~V}$ | -7 | 0 | +7 | deg |
| Function Generator Error | $25^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 80^{\circ} \mathrm{C}$ | -2 | 0 | +2 | deg |
| Function Generator Error | $25^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 105^{\circ} \mathrm{C}$ | -4 | 0 | +4 | deg |
| Function Generator Error | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq 25^{\circ} \mathrm{C}$ | -2 | 0 | +2 | deg |
| Function Generator Gain | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \Theta \mathrm{vs} \mathrm{F} / \mathrm{V}_{\text {Out }}$ | 60 | 77 | 95 | \%/V |

*Note: Deviation from nominal per Table 1 after calibration at $0^{\circ}$ and $270^{\circ}$.

## Package Lead Description

PACKAGE LEAD \#

## 20L SO <br> 16L PDIP

| 1 | 1 | $\mathrm{V}_{\mathrm{CC}}$ | Ignition or battery supply voltage. |
| :---: | :---: | :---: | :---: |
| 2 | 2 | $\mathrm{V}_{\text {REG }}$ | Voltage regulator output. |
| 3 | 3 | BIAS | Test point or zero adjustment. |
| 4, 5, 12, 13 | 5, 6, 15, 16 | Gnd | Ground Connections. |
| 6 | 8 | COS- | Negative cosine output signal. |
| 7 | 9 | SIN- | Negative sine output signal. |
| 8 | 10 | FREQ $_{\text {IN }}$ | Speed or rpm input signal. |
| 9 | 11 | SQout | Buffered square wave output signal. |
| 10 | 12 | SIN+ | Positive sine output signal. |
| 11 | 13 | COS+ | Positive cosine output signal. |
| 14 | 18 | CP- | Negative input to charge pump. |
| 15 | 19 | $\mathrm{CP}+$ | Positive input to charge pump. |
| 16 | 20 | F/V $\mathrm{V}_{\text {OUT }}$ | Output voltage proportional to input signal frequency. |
|  | 4, 7, 14, 17 | NC | No connection. |

## Typical Performance Characteristics

Figure 1: Function Generator Output Voltage vs Degrees of Deflection


Figure 2: Charge Pump Output Voltage vs Output Angle
$\mathrm{F} / \mathrm{V}_{\mathrm{OUT}}=2.0 \mathrm{~V}+2$ FREQ $\times \mathrm{C}_{\mathrm{T}} \times \mathrm{R}_{\mathrm{T}} \times\left(\mathrm{V}_{\mathrm{REG}}-0.7\right)$



Typical Performance Characteristics: continued

Figure 4: Nominal Output Deviation


## Nominal Angle vs. Ideal Angle (After calibrating at $\mathbf{1 8 0}^{\circ}$ )

Note: Temperature, voltage and nonlinearity not included.


Table 1: Function Generator Output Nominal Angle vs. Ideal Angle (After calibrating at $270^{\circ}$ )

| Ideal $\Theta$ <br> Degrees | Nominal <br> $\Theta$ Degrees | Ideal $\Theta$ <br> Degrees | Nominal <br> $\Theta$ Degrees | Ideal $\Theta$ <br> Degrees | Nominal <br> $\Theta$ Degrees | Ideal $\Theta$ <br> Degrees | Nominal <br> $\Theta$ Degrees | Ideal $\Theta$ <br> Degrees | Nominal <br> $\Theta$ Degrees | Ideal $\Theta$ <br> Degrees | Nominal <br> $\Theta$ Degrees |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 17 | 17.98 | 34 | 33.04 | 75 | 74.00 | 160 | 159.14 | 245 | 244.63 |
| 1 | 1.09 | 18 | 18.96 | 35 | 34.00 | 80 | 79.16 | 165 | 164.00 | 250 | 249.14 |
| 2 | 2.19 | 19 | 19.92 | 36 | 35.00 | 85 | 84.53 | 170 | 169.16 | 255 | 254.00 |
| 3 | 3.29 | 20 | 20.86 | 37 | 36.04 | 90 | 90.00 | 175 | 174.33 | 260 | 259.16 |
| 4 | 4.38 | 21 | 21.79 | 38 | 37.11 | 95 | 95.47 | 180 | 180.00 | 265 | 264.53 |
| 5 | 5.47 | 22 | 22.71 | 39 | 38.21 | 100 | 100.84 | 185 | 185.47 | 270 | 270.00 |
| 6 | 6.56 | 23 | 23.61 | 40 | 39.32 | 105 | 106.00 | 190 | 190.84 | 275 | 275.47 |
| 7 | 7.64 | 24 | 24.50 | 41 | 40.45 | 110 | 110.86 | 195 | 196.00 | 280 | 280.84 |
| 8 | 8.72 | 25 | 25.37 | 42 | 41.59 | 115 | 115.37 | 200 | 200.86 | 285 | 286.00 |
| 9 | 9.78 | 26 | 26.23 | 43 | 42.73 | 120 | 119.56 | 205 | 205.37 | 290 | 290.86 |
| 10 | 10.84 | 27 | 27.07 | 44 | 43.88 | 125 | 124.00 | 210 | 209.56 | 295 | 295.37 |
| 11 | 11.90 | 28 | 27.79 | 45 | 45.00 | 130 | 129.32 | 215 | 214.00 | 300 | 299.21 |
| 12 | 12.94 | 29 | 28.73 | 50 | 50.68 | 135 | 135.00 | 220 | 219.32 | 305 | 303.02 |
| 13 | 13.97 | 30 | 29.56 | 55 | 56.00 | 140 | 140.68 | 225 | 225.00 |  |  |
| 14 | 14.99 | 31 | 30.39 | 60 | 60.44 | 145 | 146.00 | 230 | 230.58 |  |  |
| 15 | 16.00 | 32 | 31.24 | 65 | 64.63 | 150 | 150.44 | 235 | 236.00 |  |  |
| 16 | 17.00 | 33 | 32.12 | 70 | 69.14 | 155 | 154.63 | 240 | 240.44 |  |  |

Note: Temperature, voltage and nonlinearity not included.

The CS8191 is specifically designed for use with air-core meter movements. It includes an input comparator for sensing an input signal from an ignition pulse or speed sensor, a charge pump for frequency to voltage conversion, a bandgap voltage regulator for stable operation, and a function generator with sine and cosine amplifiers to differentially drive the motor coils.
From the simplified block diagram of Figure 5A, the input signal is applied to the $\mathrm{FREQ}_{\text {IN }}$ lead, this is the input to a high impedance comparator with a typical positive input threshold of 2.7 V and typical hysteresis of 0.4 V . The output of the comparator, $\mathrm{SQ}_{\text {OUT }}$, is applied to the charge pump input $\mathrm{CP}+$ through an external capacitor $\mathrm{C}_{\mathrm{T}}$. When the input signal changes state, $\mathrm{C}_{\mathrm{T}}$ is charged or discharged through R3 and R4. The charge accumulated on $\mathrm{C}_{\mathrm{T}}$ is mirrored to C 4 by the Norton Amplifier circuit comprising of Q1, Q2 and Q3. The charge pump output voltage, $\mathrm{F} / \mathrm{V}_{\text {OUT }}$, ranges from 2 V to 6.3 V depending on the input signal frequency and the gain of the charge pump according to the formula:

$$
\mathrm{F} / \mathrm{V}_{\mathrm{OUT}}=2.0 \mathrm{~V}+2 \times \mathrm{FREQ} \times \mathrm{C}_{\mathrm{T}} \times \mathrm{R}_{\mathrm{T}} \times\left(\mathrm{V}_{\mathrm{REG}}-0.7 \mathrm{~V}\right)
$$

$\mathrm{R}_{\mathrm{T}}$ is a potentiometer used to adjust the gain of the $\mathrm{F} / \mathrm{V}$ output stage and give the correct meter deflection. The $\mathrm{F} / \mathrm{V}$ output voltage is applied to the function generator which generates the sine and cosine output voltages. The output voltage of the sine and cosine amplifiers are derived from the on-chip amplifier and function generator circuitry. The various trip points for the circuit (i.e., $0^{\circ}$, $90^{\circ}, 180^{\circ}, 270^{\circ}$ ) are determined by an internal resistor divider and the bandgap voltage reference. The coils are differentially driven, allowing bidirectional current flow in the outputs, thus providing up to $305^{\circ}$ range of meter deflection. Driving the coils differentially offers faster response time, higher current capability, higher output voltage swings, and reduced external component count. The key advantage is a higher torque output for the pointer.
The output angle, $\Theta$, is equal to the $F / V$ gain multiplied by the function generator gain:

$$
\Theta=\mathrm{A}_{\mathrm{F} / \mathrm{V}} \times \mathrm{A}_{\mathrm{FG}},
$$

where:

$$
\mathrm{A}_{\mathrm{FG}}=77^{\circ} / \mathrm{V}(\mathrm{typ})
$$

The relationship between input frequency and output angle is:

$$
\begin{aligned}
& \Theta=\mathrm{A}_{\mathrm{FG}} \times 2 \times \mathrm{FREQ} \times \mathrm{C}_{\mathrm{T}} \times \mathrm{R}_{\mathrm{T}} \times\left(\mathrm{V}_{\mathrm{REG}}-0.7 \mathrm{~V}\right) \\
& \text { or, } \quad \Theta=970 \times \mathrm{FREQ} \times \mathrm{C}_{\mathrm{T}} \times \mathrm{R}_{\mathrm{T}}
\end{aligned}
$$

The ripple voltage at the $\mathrm{F} / \mathrm{V}$ converter's output is determined by the ratio of $\mathrm{C}_{\mathrm{T}}$ and C 4 in the formula:

$$
\Delta \mathrm{V}=\frac{\mathrm{C}_{\mathrm{T}}\left(\mathrm{~V}_{\mathrm{REG}}-0.7 \mathrm{~V}\right)}{\mathrm{C} 4}
$$

Ripple voltage on the F/V output causes pointer or needle flutter especially at low input frequencies.
The response time of the $\mathrm{F} / \mathrm{V}$ is determined by the time constant formed by $\mathrm{R}_{\mathrm{T}}$ and C 4 . Increasing the value of C 4 will reduce the ripple on the $\mathrm{F} / \mathrm{V}$ output but will also increase the response time. An increase in response time causes a very slow meter movement and may be unacceptable for many applications.

## Design Example

Maximum meter Deflection $=270^{\circ}$
Maximum Input Frequency $=350 \mathrm{~Hz}$

## 1. Select $R_{T}$ and $C_{T}$

$$
\begin{aligned}
\Theta & =\mathrm{A}_{\mathrm{GEN}} \times \Delta_{\mathrm{F}} / \mathrm{V} \\
\Delta_{\mathrm{F} / \mathrm{V}} & =2 \times \mathrm{FREQ} \times \mathrm{C}_{\mathrm{T}} \times \mathrm{R}_{\mathrm{T}} \times\left(\mathrm{V}_{\mathrm{REG}}-0.7 \mathrm{~V}\right) \\
\Theta & =970 \times \mathrm{FREQ} \times \mathrm{C}_{\mathrm{T}} \times \mathrm{R}_{\mathrm{T}}
\end{aligned}
$$

Let $C_{T}=0.0033 \mu \mathrm{~F}$, Find $\mathrm{R}_{\mathrm{T}}$

$$
\begin{gathered}
\mathrm{R}_{\mathrm{T}}=\frac{270^{\circ}}{970 \times 350 \mathrm{~Hz} \times 0.0033 \mu \mathrm{~F}} \\
\mathrm{R}_{\mathrm{T}}=243 \mathrm{k} \Omega
\end{gathered}
$$

$\mathrm{R}_{\mathrm{T}}$ should be a $250 \mathrm{k} \Omega$ potentiometer to trim out any inaccuracies due to IC tolerances or meter movement pointer placement.

## 2. Select R3 and R4

Resistor R3 sets the output current from the voltage regulator. The maximum output current from the voltage regulator is $10 \mathrm{~mA}, \mathrm{R} 3$ must ensure that the current does not exceed this limit.

Choose R3 $=3.3 \mathrm{k} \Omega$
The charge current for $C_{T}$ is:

$$
\frac{\mathrm{V}_{\mathrm{REG}}-0.7 \mathrm{~V}}{3.3 \mathrm{k} \Omega}=1.90 \mathrm{~mA}
$$

C1 must charge and discharge fully during each cycle of the input signal. Time for one cycle at maximum frequency is 2.85 ms . To ensure that $\mathrm{C}_{\mathrm{T}}$ is discharged, assume that the ( $\mathrm{R} 3+\mathrm{R} 4$ ) $\mathrm{C}_{\mathrm{T}}$ time constant is less than $10 \%$ of the minimum input frequency pulse width.

$$
\mathrm{T}=285 \mu \mathrm{~s}
$$

Choose R4 $=1 \mathrm{k} \Omega$.
Charge time: $\quad \mathrm{T}=\mathrm{R} 3 \times \mathrm{C}_{\mathrm{T}}=3.3 \mathrm{k} \Omega \times 0.0033 \mu \mathrm{~F}=10.9 \mu \mathrm{~s}$
Discharge time: $\mathrm{T}=(\mathrm{R} 3+\mathrm{R} 4) \mathrm{C}_{\mathrm{T}}=4.3 \mathrm{k} \Omega \times 0.0033 \mu \mathrm{~F}=14.2 \mu \mathrm{~s}$

## 3. Determine C4

C4 is selected to satisfy both the maximum allowable ripple voltage and response time of the meter movement.

$$
\mathrm{C} 4=\frac{\mathrm{C}_{\mathrm{T}}\left(\mathrm{~V}_{\mathrm{REG}}-0.7 \mathrm{~V}\right)}{\mathrm{V}_{\text {RIPPLE }}(\mathrm{MAX})}
$$

With $\mathrm{C} 4=0.47 \mu \mathrm{~F}$, the $\mathrm{F} / \mathrm{V}$ ripple voltage is 44 mV .
Figure 7 shows how the CS8191 and the CS8441 are used to produce a Speedometer and Odometer circuit.


Figure 5A: Partial Schematic of Input and Charge Pump


Figure 5B: Timing Diagram of FREQ ${ }_{\text {IN }}$ and $\mathrm{I}_{\mathrm{C}_{\mathrm{P}}}$


Figure 6
R1-3.9, 500mW
R2-10k $\Omega$
R3-3k $\Omega$
R4-1k $\Omega$
$\mathrm{R}_{\mathrm{T}}$ - Trim Resistor +/-20 PPM/DEG. C
C1-0.1 $\mu \mathrm{F}$
C2 - With CS-8441 application, $10 \mu \mathrm{~F}$
C3-0.1 $\mu \mathrm{F}$
C4-0.47 $\mu \mathrm{F}$
$\mathrm{C}_{\mathrm{T}}-0.0033 \mu \mathrm{~F},+/-30 \mathrm{PPM} /{ }^{\circ} \mathrm{C}$
D1-1A, 600 PIV
D2-50V, 500mW Zener

Note 1: The product of $C_{T}$ and $R_{T}$ have a direct effect on gain and therefore directly effect temperature compensation.
Note 2: C4 Range; 20 pF to $.2 \mu \mathrm{~F}$.
Note 3: R4 Range; $100 \mathrm{k} \Omega$ to $500 \mathrm{k} \Omega$.


Figure 7

Note 4: The IC must be protected from transients above 60 V and reverse battery conditions.
Note 5: Additional filtering on the $\mathrm{FREQ}_{\text {IN }}$ lead may be required.

In some cases a designer may wish to use the CS8191 only as a driver for an air-core meter having performed the $\mathrm{F} / \mathrm{V}$ conversion elsewhere in the circuit.
Figure 8 shows how to drive the CS8191 with a DC voltage ranging from 2 V to 6 V . This is accomplished by forcing a voltage on the $\mathrm{F} / \mathrm{V}_{\text {OUT }}$ lead. The alternative scheme shown in figure 9 uses an external op amp as a buffer and operates over an input voltage range of 0 V to 4 V .


Figure 8. Driving the CS8191 from an external DC voltage.

An alternative solution is to use the CS4101 which has a separate function generator input lead and can be driven directly from a DC source. Figure 8 and 9 are not temperature compensated.


Figure 9. Driving the CS8191 from an external DC voltage using an Op Amp Buffer.
PACKAGE DIMENSIONS IN mm (INCHES)

| Lead Count | $\frac{\text { Metric }}{}$ | $\frac{\text { English }}{}$ |
| :--- | :--- | :--- |
| $\frac{\text { Max }}{19.69}$ | $\frac{\text { Min }}{18.67}$ | $\frac{\text { Max }}{.775}$ |
| $\frac{\text { Min }}{.735}$ |  |  |
| 16L PDIP (internally fused leads) | $\frac{19}{12.60}$ | $\frac{.512}{.496}$ |

PACKAGE THERMAL DATA

| Thermal Data |  | 16L PDIP* | 20L SOIC* |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{R}_{\text {©JC }}$ | typ | 15 | 9 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {©JA }}$ | typ | 50 | 55 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

*Internally Fused Leads

Plastic DIP (N); 300 mil wide


Surface Mount Wide Body (DW); 300 mil wide


| Ordering Information |  |
| :---: | :---: |
| Part Number | Description |
| CS8191XNF16 | 16L PDIP (internally fused leads) |
| CS8191XDWF20 | 20L SOIC (internally fused leads) |
| CS8191XDWFR20 | 20L SOIC (internally fused leads) (tape $\mathcal{E}$ reel) |

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