

5A Adjustable Linear Regulator

Description

The CS5205A-1 linear regulator provides 5A at an adjustable voltage with an accuracy of $\pm 1\%$. Two external resistors are used to set the output voltage within a 1.25V to 13V range.

The regulator is intended for use as a post regulator and microprocessor supply. The fast loop response and low dropout voltage make this regulator ideal for applications where low voltage operation and good transient response are important.

The circuit is designed to operate with dropout voltages as low as 1V

depending on the output current level. The maximum quiescent current is only 10mA at full load.

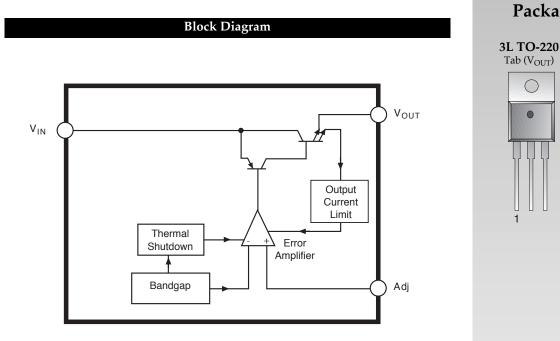
The regulator is fully protected against overload conditions with protection circuitry for Safe Operating Area (SOA), overcurrent and thermal shutdown.

The CS5205A-1 is pin compatible with the LT1084 family of linear regulators but has lower dropout voltage.

The regulator is available in TO-220 and surface mount D^2 packages.

Features

- **Output Current to 5A**
- **Output Trimmed to +/- 1%**
- **Dropout Voltage** 1.15V @ 5A
- **Fast Transient Response**
- **Fault Protection Circuitry Thermal Shutdown Overcurrent Protection** Safe Area Protection





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Package Options

 \bigcirc

3L D²PAK

1 Adj

3 VIN

VOUT 2

Absolute Maximum Ratings

Suj	pply	Vo
Op	erati	ng
-		-

CS5205A-1

Supply Voltage, V _{CC}	
Operating Temperature Range	
Junction Temperature	
Storage Temperature Range	
Lead Temperature Soldering	
Wave Solder (through hole styles only)	10 sec. max, 260°C peak
Reflow (SMD styles only)	60 sec. max above 183°C, 230°C peak

 $Electrical \ Characteristics: \ C_{IN} = 10 \mu F, \ C_{OUT} = 22 \mu F \ Tantalum, \ V_{IN} - V_{OUT} = 3V, \ V_{IN} \le 15V, \ 0^{\circ}C \le T_A \le 70^{\circ}C, \ T_J \le +150^{\circ}C, \ T_J \ T_J$

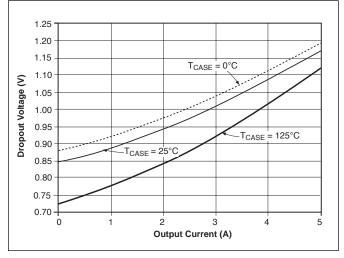
unless otherwise specified, $I_{full load} = 5A$.				
TEST CONDITIONS	MIN	ТҮР	MAX	UNIT
$V_{IN}-V_{OUT}=1.5V$; $V_{Adj} = 0V$ $10mA \le I_{OUT} \le 5A$	1.241 (-1%)	1.254	1.266 (+1%)	V
$1.5V \le V_{IN} - V_{OUT} \le 6V$; $I_{OUT} = 10mA$		0.04	0.20	%
V _{IN} -V _{OUT} =1.5V; 10mA≤I _{OUT} ≤5A		0.08	0.4	%
$I_{OUT}=5A; T_J \ge 25^{\circ}C$		1.15	1.25	V
$V_{IN}-V_{OUT}=3V; T_J \ge 25^{\circ}C$ $V_{IN}-V_{OUT}=9V$	5.5	8.5 1.0		A A
V _{IN} -V _{OUT} =7V		1.2	6	mA
		50	100	μA
1.5V≤V _{IN} −V _{OUT} ≤4V; 10mA≤I _{OUT} ≤5A		0.2	5.0	μΑ
30ms pulse; T _A =25°C		0.003		%W
f=120Hz; C _{Adj} =25µF; I _{OUT} =5A		82		dB
		0.5		%
10Hz≤f≤10kHz; T _A =25°C		0.003		%V _{OUT}
	150	180		°C
		25		°C
	$\label{eq:starsest} \begin{array}{l} \hline \textbf{TEST CONDITIONS} \\ \hline \textbf{V}_{IN} - \textbf{V}_{OUT} = 1.5 \textbf{V}; \ \textbf{V}_{Adj} = 0 \textbf{V} \\ 10 \textbf{mA} \leq \textbf{I}_{OUT} \leq 5 \textbf{A} \\ \hline 1.5 \textbf{V} \leq \textbf{V}_{IN} - \textbf{V}_{OUT} \leq 6 \textbf{V}; \ \textbf{I}_{OUT} = 10 \textbf{mA} \\ \hline \textbf{V}_{IN} - \textbf{V}_{OUT} = 1.5 \textbf{V}; \\ 10 \textbf{mA} \leq \textbf{I}_{OUT} \leq 5 \textbf{A} \\ \hline \textbf{I}_{OUT} = 5 \textbf{A}; \ \textbf{T}_{J} \geq 25^{\circ} \textbf{C} \\ \hline \textbf{V}_{IN} - \textbf{V}_{OUT} = 3 \textbf{V}; \ \textbf{T}_{J} \geq 25^{\circ} \textbf{C} \\ \hline \textbf{V}_{IN} - \textbf{V}_{OUT} = 9 \textbf{V} \\ \hline \textbf{V}_{IN} - \textbf{V}_{OUT} = 7 \textbf{V} \\ \hline 1.5 \textbf{V} \leq \textbf{V}_{IN} - \textbf{V}_{OUT} \leq 4 \textbf{V}; \\ 10 \textbf{mA} \leq \textbf{I}_{OUT} \leq 5 \textbf{A} \\ \hline \textbf{30} \textbf{ms} \textbf{ pulse}; \ \textbf{T}_{A} = 25^{\circ} \textbf{C} \\ \textbf{f} = 120 \textbf{H}z; \ \textbf{C}_{Adj} = 25 \mu \textbf{F}; \ \textbf{I}_{OUT} = 5 \textbf{A} \end{array}$	$\begin{array}{c c} V_{IN}-V_{OUT}=1.5V; V_{Adj}=0V & 1.241 \\ 10mA \leq I_{OUT} \leq 5A & (-1\%) \\ 1.5V \leq V_{IN}-V_{OUT} \leq 6V; I_{OUT}=10mA & \\ V_{IN}-V_{OUT}=1.5V; \\ 10mA \leq I_{OUT} \leq 5A & \\ I_{OUT}=5A; T_J \geq 25^{\circ}C & \\ V_{IN}-V_{OUT}=3V; T_J \geq 25^{\circ}C & 5.5 \\ V_{IN}-V_{OUT}=9V & \\ V_{IN}-V_{OUT}=7V & \\ 1.5V \leq V_{IN}-V_{OUT} \leq 4V; \\ 10mA \leq I_{OUT} \leq 5A & \\ 30ms \text{ pulse}; T_A=25^{\circ}C & \\ f=120Hz; C_{Adj}=25\mu F; I_{OUT}=5A & \\ 10Hz \leq f \leq 10kHz; T_A=25^{\circ}C & \\ \end{array}$	$\begin{array}{ c c c c c } \hline \text{TEST CONDITIONS} & \text{MIN} & \text{TYP} \\ \hline & & & & & & & & & & & & & & & & & &$	$\begin{tabular}{ c c c c c c } \hline TEST CONDITIONS & MIN & TYP & MAX \\ \hline Test CONDITIONS & MIN & TYP & MAX \\ \hline V_{IN}-V_{OUT}=1.5V; V_{Adj} = 0V & 1.241 & 1.254 & 1.266 & (-1\%) & (+1\%) & (+1\%) & (+1\%) & (+1\%) & (+1\%) & (-1$

Note 1: Load regulation and output voltage are measured at a constant junction temperature by low duty cycle pulse testing. Changes in output voltage due to thermal gradients or temperature changes must be taken into account separately.

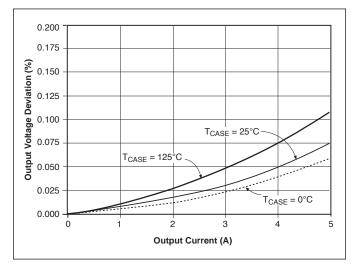
Note 2: Specifications apply for an external Kelvin sense connection at a point on the output pin 1/4'' from the bottom of the package.

Note 3: Dropout voltage is a measurement of the minimum input/output differential at full load.

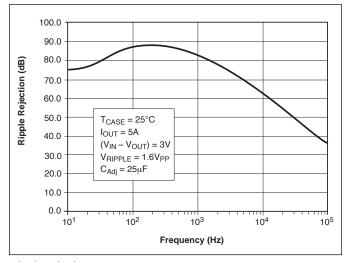
Package Pin Description			
PACKAGE PIN # PIN SYMBOL FUNCTION		FUNCTION	
D ² PAK	3L TO-220		
1	1	Adj	Adjust pin (low side of the internal reference).
2	2	V _{OUT}	Regulated output voltage (case).
3	3	V _{IN}	Input voltage.



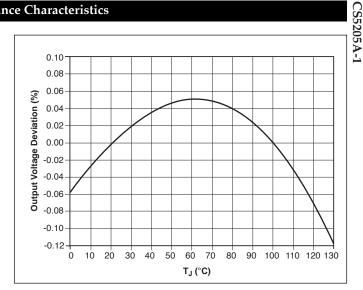
Dropout Voltage vs. Output Current



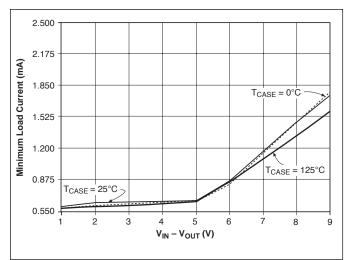
Load Regulation vs. Output Current



Ripple Rejection vs. Frequency



Reference Voltage vs. Temperature



Minimum Load Current

CS5205A-1

The CS5205A-1 linear regulator provides an adjustable voltage at currents up to 5A. The regulator is protected against short circuit, and include thermal shutdown and safe area protection (SOA) circuitry. The SOA protection circuitry decreases the maximum available output current as the input-output differential voltage increases.

The CS5205A-1 has a composite PNP-NPN output transistor and requires an output capacitor for stability. A detailed procedure for selecting this capacitor is included in the Stability Considerations section.

Adjustable Operation

The adjustable regulator (CS5205A-1) has an output voltage range of 1.25V to 13V. An external resistor divider sets the output voltage as shown in Figure 1. The regulator maintains a fixed 1.25V (typical) reference between the output pin and the adjust pin.

A resistor divider network R1 and R2 causes a fixed current to flow to ground. This current creates a voltage across R2 that adds to the 1.25V across R1 and sets the overall output voltage. The adjust pin current (typically 50 μ A) also flows through R2 and adds a small error that should be taken into account if precise adjustment of V_{OUT} is necessary.

The output voltage is set according to the formula:

$$V_{OUT} = V_{REF} \times \left(\frac{R1 + R2}{R1}\right) + I_{Adj} \times R2$$

The term $I_{Adj} \times R2$ represents the error added by the adjust pin current.

R1 is chosen so that the minimum load current is at least 10mA. R1 and R2 should be the same type, e.g. metal film for best tracking over temperature. The adjust pin is bypassed to improve the transient response and ripple rejection of the regulator.

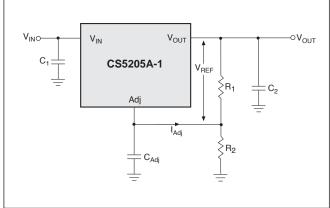


Figure 1. Resistor divider scheme for the adjustable version.

Stability Considerations

The output or compensation capacitor helps determine three main characteristics of a linear regulator: start-up delay, load transient response and loop stability.

The capacitor value and type is based on cost, availability, size and temperature constraints. A tantalum or aluminum electrolytic capacitor is best, since a film or ceramic capaci-

tor with almost zero ESR, can cause instability. The aluminum electrolytic capacitor is the least expensive solution. However, when the circuit operates at low temperatures, both the value and ESR of the capacitor will vary considerably. The capacitor manufacturers data sheet provides this information.

A 22μ F tantalum capacitor will work for most applications, but with high current regulators such as the CS5205A-1 the transient response and stability improve with higher values of capacitor. The majority of applications for this regulator involve large changes in load current so the output capacitor must supply the instantaneous load current. The ESR of the output capacitor causes an immediate drop in output voltage given by:

$$\Delta V = \Delta I \times ESR$$

For microprocessor applications it is customary to use an output capacitor network consisting of several tantalum and ceramic capacitors in parallel. This reduces the overall ESR and reduces the instantaneous output voltage drop under load transient conditions. The output capacitor network should be as close as possible to the load for the best results.

Protection Diodes

When large external capacitors are used with a linear regulator it is sometimes necessary to add protection diodes. If the input voltage of the regulator gets shorted, the output capacitor will discharge into the output of the regulator. The discharge current depends on the value of the capacitor, the output voltage and the rate at which $V_{\rm IN}$ drops. In the CS5205A-1 linear regulator, the discharge path is through a large junction and protection diodes are not usually needed. If the regulator is used with large values of output capacitance and the input voltage is instantaneously shorted to ground, damage can occur. In this case, a diode connected as shown in Figure2 is recommended.

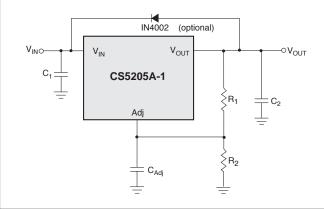


Figure 2. Protection diode scheme for adjustable output regulator.

Output Voltage Sensing

Since the CS5205A-1 is a three terminal regulator, it is not possible to provide true remote load sensing. Load regulation is limited by the resistance of the conductors connecting the regulator to the load. Best load regulation occurs when R1 is connected directly to the output pin of the regulator as shown in Figure 3. If R1 is connected to the load, R_C is multiplied by the divider ratio and the effective resistance between the regulator and the load becomes

$$R_{C} \times \left(\frac{R1 + R2}{R1}\right)$$

R_{C} = conductor parasitic resistance

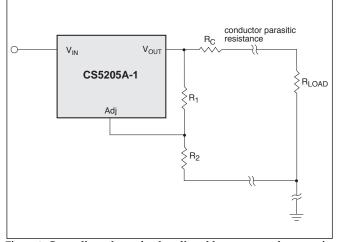


Figure 3. Grounding scheme for the adjustable output regulator to minimize parasitics.

Calculating Power Dissipation and Heat Sink Requirements

The CS5205A-1 linear regulator includes thermal shutdown and safe operating area circuitry to protect the device. High power regulators such as these usually operate at high junction temperatures so it is important to calculate the power dissipation and junction temperatures accurately to ensure that an adequate heat sink is used.

The case is connected to V_{OUT} on the CS5205A-1, electrical isolation may be required for some applications. Thermal compound should always be used with high current regulators such as these.

The thermal characteristics of an IC depend on the following four factors:

- 1. Maximum Ambient Temperature T_A (°C)
- 2. Power dissipation P_D (Watts)
- 3. Maximum junction temperature T_{I} (°C)
- 4. Thermal resistance junction to ambient $R_{\Theta JA}$ (C/W)

These four are related by the equation

$$\Gamma_{\rm I} = T_{\rm A} + P_{\rm D} \times R_{\Theta \rm IA} \tag{1}$$

The maximum ambient temperature and the power dissipation are determined by the design while the maximum junction temperature and the thermal resistance depend on the manufacturer and the package type. The maximum power dissipation for a regulator is:

 $P_{D(max)} = \{V_{IN(max)} - V_{OUT(min)}\}I_{OUT(max)} + V_{IN(max)}I_Q$

CS5205A-1

(2)

where

 $V_{IN(max)}$ is the maximum input voltage,

V_{OUT(min)} is the minimum output voltage,

I_{OUT(max)} is the maximum output current, for the application

 I_Q is the maximum quiescent current at $I_{OUT}(max)$.

A heat sink effectively increases the surface area of the package to improve the flow of heat away from the IC and into the surrounding air.

Each material in the heat flow path between the IC and the outside environment has a thermal resistance. Like series electrical resistances, these resistances are summed to determine $R_{\Theta JA}$, the total thermal resistance between the junction and the surrounding air.

- 1. Thermal Resistance of the junction to case, $R_{\Theta IC}(^{\circ}C/W)$
- 2. Thermal Resistance of the case to Heat Sink, R_{OCS} (°C/W)
- 3. Thermal Resistance of the Heat Sink to the ambient air, $R_{\Theta SA}$ (°C/W)

These are connected by the equation:

$$R_{\Theta JA} = R_{\Theta JC} + R_{\Theta CS} + R_{\Theta SA} \tag{3}$$

The value for $R_{\Theta JA}$ is calculated using equation (3) and the result can be substituted in equation (1).

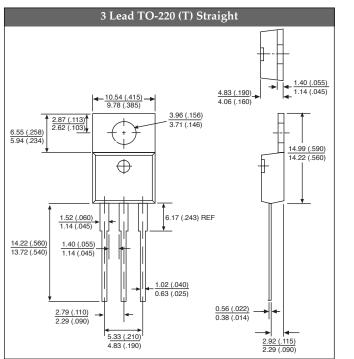
The value for $R_{\Theta JC}$ is normally quoted as a single figure for a given package type based on an average die size. For a high current regulator such as the CS5205A-1 the majority of the heat is generated in the power transistor section. The value for $R_{\Theta SA}$ depends on the heat sink type, while $R_{\Theta CS}$ depends on factors such as package type, heat sink interface (is an insulator and thermal grease used?), and the contact area between the heat sink and the package. Once these calculations are complete, the maximum permissible value of $R_{\Theta JA}$ can be calculated and the proper heat sink selected. For further discussion on heat sink selection, see application note "Thermal Management for Linear Regulators." **Package Specification**

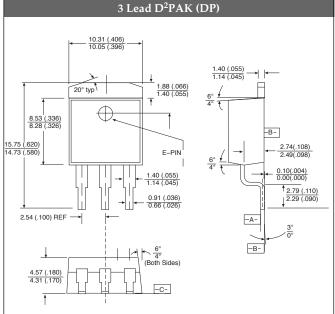
PACKAGE DIMENSIONS IN mm(INCHES)

PACKAGE THERMAL DATA

Therma	l Data	3L TO-220	3L D ² PAK	
R _{ØJC}	typ	1.6	1.6	°C/W
R _{OJA}	typ	50	10 - 50*	°C/W
		 1 properties of sub		

*Depending on thermal properties of substrate. $R_{\Theta JA} = R_{\Theta JC} + R_{\Theta CA}$





Ordering Information			
Part Number	Туре	Description	
CS5205A-1GT3	5A, adj. output	3L TO-220 Straight	
CS5205A-1GDP3	5A, adj. output	3L D ² PAK	
CS5205A-1GDPR3	5A, adj. output	3L D ² PAK (<i>tape & reel</i>)	

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